

**SOFTSWITCHING PWM REGULATOR****R.VIDYASAGAR and M.M.IRFAN**

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**ABSTRACT**

This paper proposes soft switching capacitor pulse width modulation converter. The converter is a combination of switching capacitor converter and PWM regulator. The capacitor in the converter serves as the component of processing energy and meanwhile the output voltage is regulated by the duty cycle. The main switches achieve zero-voltage-switching and the rectifier diode realizes zero-current-switching. A Simulink model is developed for verifying in the proposed analytical derivations.

**Keywords-** *switching capacitor converter; PWM regulator; soft switching.*

**I. INTRODUCTION**

The classical switched-mode converter has been a popular topology for dc/dc power conversion because it is technologically mature and is easy to use. One of the main disadvantages is that the size of their energy storage components, namely, capacitor and inductor, are very dependent on the switching frequency. Switched-capacitor

converters [1] do not require any inductor. Therefore, much research has been carried out to develop such inverters during the last decade or so. Usually, these converters require a large number of transistors to change the topology of the circuit by connecting a switching capacitor between the source and load [2], [3]. The voltage regulation of such converter is also difficult because the magnitude of the output voltage must be a fraction or a multiple of the source voltage [4], [5]. In order to regulate the converter, the switching capacitor's charge and discharge characteristics must also be taken into account and, thus, the switching device's duty ratios used to control the amount of power through the switching capacitor. The drawback of this converter is that the transistor's on-state resistance and the equivalent series resistance of the capacitor must have the same order of magnitude as the capacitor's impedance. Such constraint would decrease the efficiency of the converter.

Voltage regulators have recently been developed for getting a sub-1-V supply voltage needed in microprocessors [6]. These converter, purposely designed for high load current and fast dynamics, are still in the development phase for answering

though requirements. The switched-capacitor converters, proposed in the 1990s, can provide any steep conversion ratio (a tutorial on these circuits can be found in [7]). However, they operate with a relatively low efficiency and put di/dt challenges in the charging path of the capacitor.

For traditional converters (such as Buck, Boost, Buck-Boost), the output voltage can be regulated by the duty cycle and we call them PWM regulators. The inductor is in series with the main power delivery loop and acts as the component of transferring energy. As well known, the inductor current slew rate is constrained, which limits the energy delivery speed from input to output [8]. To meet the requirement of high di/dt in some occasions, someone proposes the switching capacitor (SC) converter, which employs the capacitor as the main component of power delivery. The energy can be transferred from input to output fast. Therefore, it achieves good dynamic performance. And due to the absence of the inductor, the weight and volume decreases a lot. However, it has some drawbacks: 1) the output voltage is fixed and can't be regulated; 2) the switch turn-on inrush current is large [9-12]. In order to combine the advantages of above two kinds of converter and overcome their shortcomings, a switching capacitor regulator is presented [13]. The capacitor in the converter serves as the component of processing energy and meanwhile the output voltage is regulated by the duty cycle.

## II. ANALYSIS OF THE PROPOSED CONVERTER NEGLIGIBLE LEAKAGE INDUCTOR

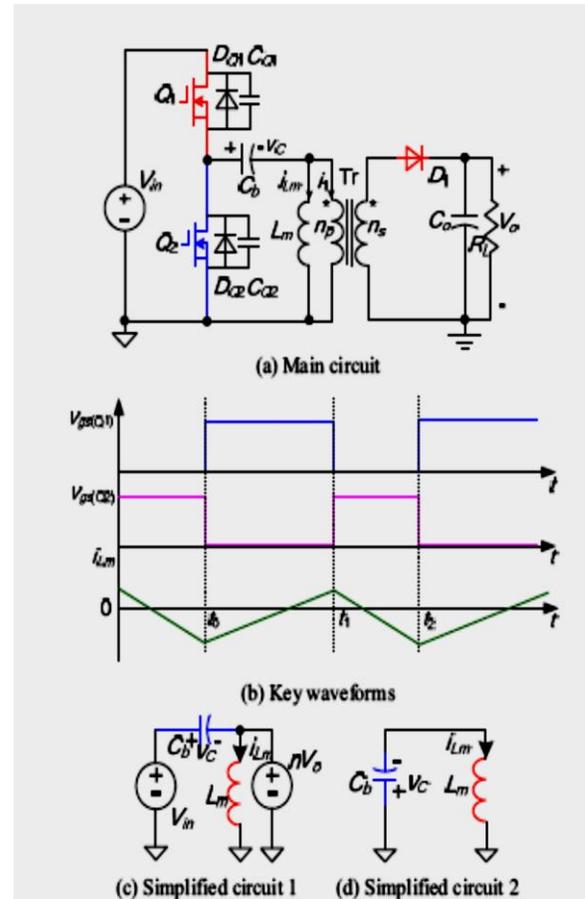


Fig.1. Isolated switching capacitor regulator.

Fig.1 shows the proposed isolated switching capacitor regulator's main circuit, key waveforms and simplified circuits.

Stage 1 ( $[t_0, t_1]$ ) (Fig.1(c)):  $Q_1$  is turned on. The output voltage  $V_o$  reflects to the primary side and is in series with the capacitor  $C_b$ , and then in parallel with the input voltage  $V_{in}$ . It acts as a switching capacitor converter and has good transient response.

Stage 2 ( $[t_1, t_2]$ ) (Fig.1(d)):  $Q_1$  is turned off and  $Q_2$  is turned on. The transformer is reset, and the output voltage is regulated by the duty cycle of  $Q_2$ . The converter acts as a PWM regulator.

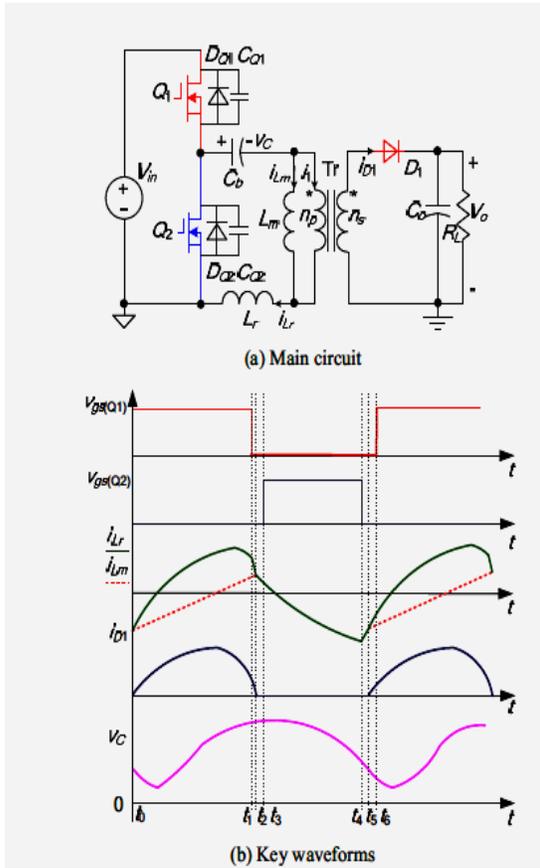


Fig.2. The isolated switching capacitor regulator with the leakage inductor

According to the analysis, it is seen that the converter is the combination of a switching capacitor converter and a PWM regulator. It has good dynamic characteristics and capability of regulating the output voltage. From the above analysis, the conversion ratio from input to output can be derived:

$$V_o = \frac{DV_m}{n} \quad (1)$$

Where  $D$  is the duty cycle of  $Q2$ ,  $n$  is the turn ratio from primary to secondary side.

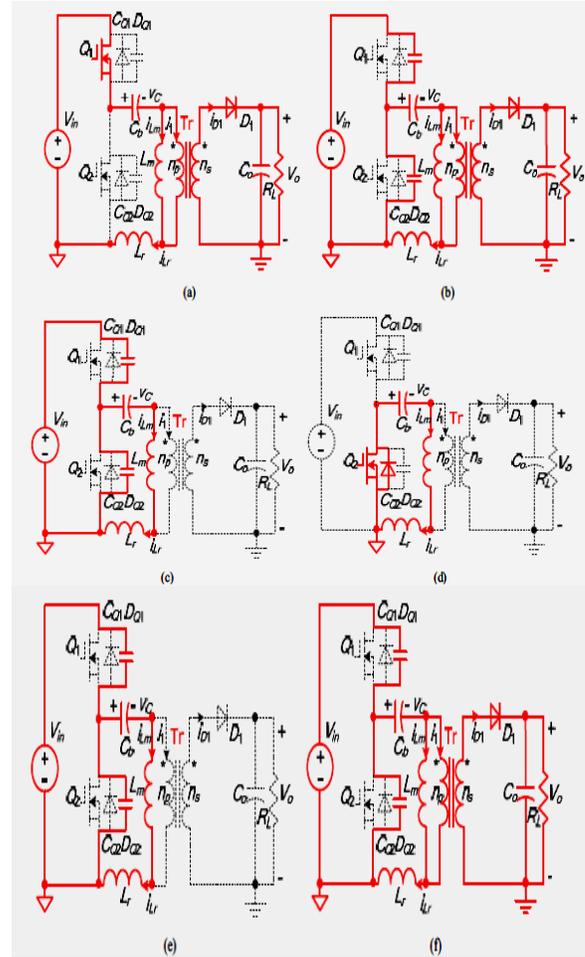


Fig.3 The equivalent circuits

### III. ANALYSIS OF THE PROPOSED CONVERTER WITH NON-NEGLECTIBLE LEAKAGE INDUCTORS

In practical applications, the transformer is not ideal and will introduce a leakage inductor. If the leakage inductor is large and can't be ignored, the leakage inductor will be resonant with the blocking capacitor. The main circuit and key waveforms are shown by Fig.4 And Fig.5 shows the equivalent circuits of all the modes.

Stage 1 ( $[t_0, t_1]$ ) (Fig.3(a)):  $Q1$  is turned on. The block capacitor  $C_b$  is resonant with the leakage inductor  $L_r$ .

The magnetizing current  $iLm$  rises linearly.

Stage 2 ( $[t1, t2]$ ) (Fig.3(b)): The switch  $Q1$  is turned off. The leakage inductor current  $iLr$  charges  $Q1$ 's parasitic capacitor  $CQ1$  and discharges  $Q2$ 's parasitic capacitor  $CQ2$ .

Stage 3 ( $[t2, t3]$ ) (Fig.3(c)): At  $t2$ ,  $iLr$  is equal to the magnetizing current  $iLm$ . The diode  $D1$  achieves zero-current switching. The primary side is separate from the secondary side. The transformer works as an inductor.

4) Stage 4 ( $[t3, t4]$ ) (Fig.3(d)): At  $t3$ , the voltage of  $CQ2$  is discharged to zero and  $DQ2$  starts to conduct. After this moment  $Q2$  can achieve zero-voltage-switching. In this stage, the block capacitor is resonant with the magnetic inductor and leakage inductor.

TABLE I COMPARISON BETWEEN THE PROPOSED CONVERTER AND OTHER SIMILAR TOPOLOGIES

Topology	Isolated switching capacitor regulator (proposed)	Flyback converter	Asymmetrical half-bridge flyback converter[8]	LLC resonant converter (half-bridge)[9]
DC gain	$V_o = \frac{D}{n} V_n$	$V_o = \frac{D}{(1-D)n} V_n$	$V_o = \frac{D}{n} V_n$	Related to D and frequency
Voltage stress	$V_n$	$V_n + nV_o$	$V_n$	$V_n$
Soft switching	ZVS	no	ZVS	ZVS
Switches	2 active switches 1 diode	1 active switch 1 diode	2 active switches 1 diode	2 active switches 2 diodes
Magnetic components	transformer	transformer	transformer	transformer resonant inductor

5) Stage 5 ( $[t4, t5]$ ) (Fig.3(e)): At  $t4$ ,  $Q2$  is switched off, and  $iLr$  charges  $CQ2$  and discharges  $CQ1$ .

6) Stage 6 ( $[t5, t6]$ ) (Fig.3(f)): At  $t5$ , the voltage of the secondary side is equal to the output voltage and  $D1$  starts to conduct.

7) Stage 7 ( $[t6, \dots]$ ) (Fig.3(g)): At  $t6$ , the voltage of  $CQ1$  is discharged to zero and

$DQ1$  starts to conduct. After this moment  $Q1$  can achieve zero-voltage-switching.

Table.1 shows the comparison between the proposed isolated switching capacitor regulator and other similar converters. The proposed converter has the following

advantages: low voltage stress, few magnetic components and switches, and achievement of zero-voltage-switching.

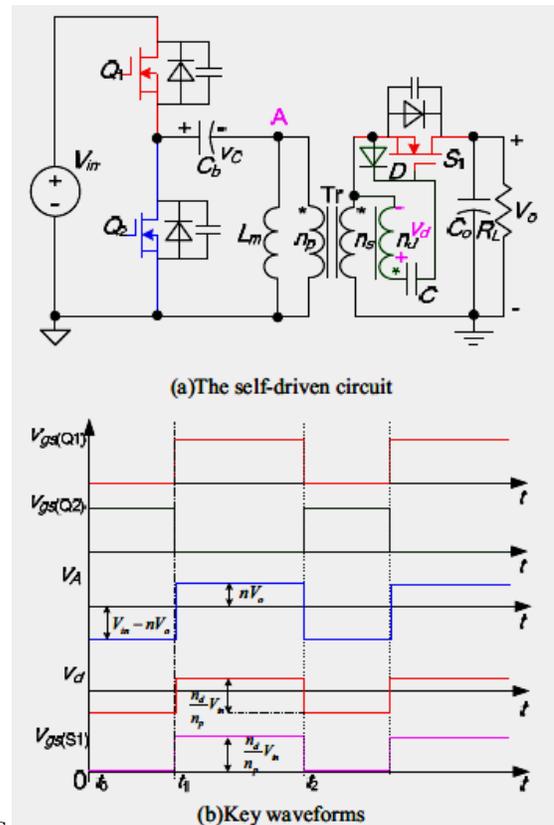


Fig.4 The self-driven method

#### IV. SELF-DRIVEN SYNCHRONOUS RECTIFIER

In order to improve efficiency in the large output current application, synchronous rectifier (SR) should be used. Compared to external-driven method, the SR self-driven method can

reduce SR drive loss and body diode conduction loss. Therefore, self-driven method is employed in the proposed circuit to further improve efficiency and increase power density. By adding an additional winding and blocking capacitor [10], we can obtain the appropriate driving signal for the synchronous rectifier. The main circuit and key waveforms are shown in Fig.4.

Stage 1( $[t_0, t_1]$ ):  $Q_2$  is switched on, and  $v_d$  is negative. The diode  $D$  conducts and the capacitor  $C$  is charged. So in this stage  $S_1$  is switched off.

Stage 2( $[t_1, t_2]$ ):  $Q_2$  is switched off and  $Q_1$  is switched on  $v_d$  is positive and  $S_1$  is switched on.

By adjusting the turns number of the additional winding, the SR loss is further reduced.

## V. SIMULATION RESULTS

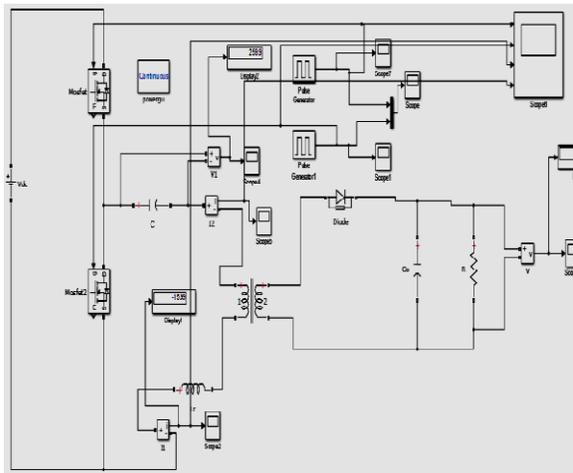


Fig.5. simulation circuit

Fig.5. shows simulation circuit for the proposed converter. here zero voltage switching is used for main switches and zero current switching referred for rectifier diode.

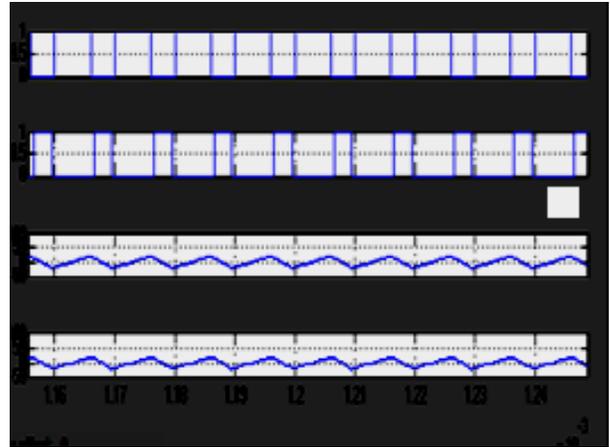


Fig.6. output wave forms

In Fig.6. one and two wave shapes represent the pulses generated for the main switches.

Waves 4 and 5 represent  $L_r$  and  $L_m$ .

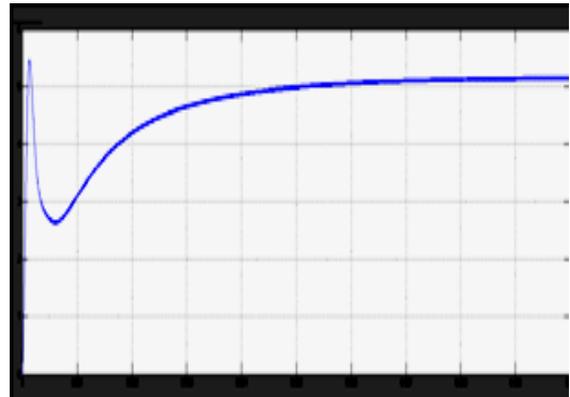


Fig.7. output voltage wave form

Fig.7. shows the output voltage converted from the converter for an input voltage of 400V the converter regulated to the 5Vdc.

## VI. CONCLUSION

An isolated switching capacitor regulator is proposed in this paper. The proposed converter has the following advantages:  
 1) Fast transient response and the output

voltage can be regulated as well. 2) The main switches achieve zero voltage-switching and the rectifier diode realizes zero-current-switching. 3) Self driven synchronous rectifier can be employed to improve efficiency.

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